

一. (20分)

- (1) 由飽和粘土單體中之體積改變率 $= (k_x \frac{\partial^2 h}{\partial x^2} + k_y \frac{\partial^2 h}{\partial y^2} + k_z \frac{\partial^2 h}{\partial z^2}) dx dy dz$, 試導下列 Terzaghi 之斥密 (consolidation) 基本公式。

$$\frac{\partial u}{\partial t} = \left(\frac{k(1+e)}{a_v \gamma_w} \right) \frac{\partial^2 u}{\partial z^2}$$

- (2) 何謂離心含水量 (Centrifuge Moisture Equivalent), 並述其工程實務上之應用。

二. (30分)

- (1) 於 6m 長鋼板樁排成之擋土牆, 牆後土壤為內摩擦角 32° , 單位重 1.87 t/m^3 之砂質土壤, 地下水位於牆頂下 2.0m。鋼板樁頂部下 1.3m 處, 設置直徑 20mm 之鋼桿, 其間隔為 1m 時, 試求鋼板樁之土中應有深度。

備註: $\sin 32^\circ = 0.53, \quad \tan 32^\circ = 0.625$
 $\gamma' = 1.05 \text{ t/m}^3$

鋼桿之最大抗張強度 $= 1.2 \text{ t/cm}^2$

- (2) 某填土工程所使用之土壤為含有通過 200 號篩 4~8% 之粗粒土壤。試述工地压实設備之適用性, 並述填土工程前後, 在試驗室及工地宜作何種試驗, 以提升品質。
- (3) 於內摩擦角 32° , 孔隙比 0.55, 土粒比重 2.66 之均等質砂層, 試求砂層完全浸水情況時, 安全係數 $= 1.5$ 之斜面角度。

Problem 3: Housel (1929) proposed a method for obtaining the soil-bearing capacity of a footing resting on a cohesive soil for a given settlement, S . According to this procedure, the total load carried by a footing of area A and perimeter P can be given by

$$Q = Aq + Ps$$

where q = compression stress below the footing
 s = unit shear stress at the perimeter

The results of two plate load tests are given in the following table.

plate diameter, D (m)	Total load, Q (KN)	settlement (mm)
0.305	32.2	20
0.610	71.8	20

A square column foundation has to be constructed to carry a total load of 815 KN. The tolerable settlement is 20 mm. Determine the size of the foundation. (10 %)

Problem 4: Peck (1969) suggested using design pressure envelopes for braced cut in sand and clay to be shown in Figure P4.1. Now Refer to Figure P4.2. Given: $\gamma = 17.5 \text{ KN/m}^3$, $C = 30 \text{ KN/m}^2$, and center-to-center spacing of struts = 5 m. Draw the earth pressure envelope (shear force diagram) and determine the strut loads at levels A, B, and C. (20 %)

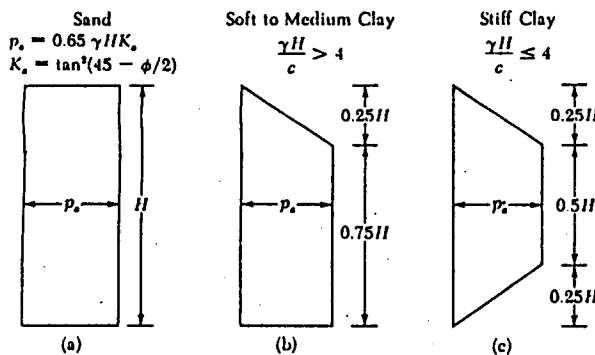


Figure P4.1 Peck's pressure envelopes for braced cuts in sand and clay [note: in Figure (b), $p_s = \gamma H [1 - (4c/\gamma H)]$ or about $0.3\gamma H$, whichever is higher; in Figure (c), $p_s = 0.2\gamma H$ to $0.4\gamma H$, with an average $0.3\gamma H$]

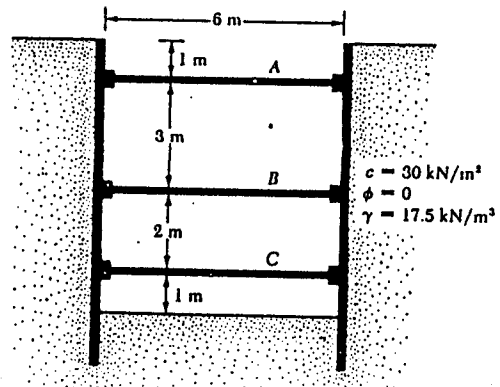


Figure P4.2

Problem 5: λ -Method was proposed by Vijayvergiya and Focht (1972), and the total frictional resistance can be given as

$$Q_s = \rho L f_{av} = \rho L \lambda (\bar{\sigma}'_v + 2C_u)$$

where $\bar{\sigma}'_v$ = mean effective vertical stress for entire embedment length

C_u = mean undrained shear strength ($\phi = 0$ concept)

A concrete pile 405 mm x 405 mm in cross section in Figure P5. Determine the allowable load that the pile can carry (FS = 3). Use the λ -method for determination of the skin resistance. Assume $\lambda = 0.16$ and the compressive strength of concrete pile is 210.0 Kg/cm^2 , $\gamma_v = 10 \text{ KN/m}^3$. (20 %)

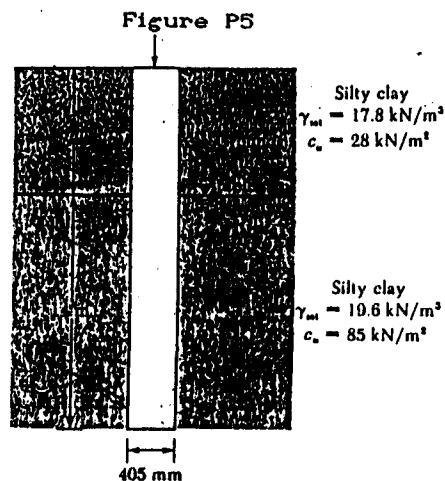


Figure P5